

26. ORGANIC CARBON, REDUCED SULFUR, AND IRON RELATIONSHIPS IN SEDIMENTS OF THE PERU MARGIN, SITES 680 AND 688¹

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ABSTRACT

Organic-carbon-rich anoxic sediments from the continental shelf (Site 680) and the lower continental slope (Site 688) off Peru were studied to determine factors controlling the accumulation of reduced sulfur. High concentrations of organic matter in diatomaceous muds, its thermal immaturity, and the presence of abundant hydrogen-containing organic compounds lead to the conclusion that organic matter is not limiting for reduced sulfur formation. Rather, high degrees of iron pyritization at Site 680 limit pyrite accumulation in sediments from this shelf site. The low degree of iron pyritization and nearly complete reduction of dissolved sulfate at Site 688 suggest that a lack of interstitial sulfate is limiting pyrite formation there. Although factors that limit the formation of sedimentary iron sulfide are different at each site, the resulting average reduced-sulfur concentrations are remarkably similar (0.85 wt.% at Site 680 and 0.86 wt.% at Site 688). Carbon to sulfur (C/S) ratios are higher in samples containing in excess of 3 wt.% organic carbon than the average of 2.8 in normal marine sediments and have been primarily influenced by variations in organic matter concentrations.

INTRODUCTION

Bacterially mediated reduction of sulfate during oxidation of organic matter in marine sediments results in the production of hydrogen sulfide. A portion of the reduced sulfur is retained in iron sulfide minerals until the sediment has been exposed to weathering. Although the processes of sulfate reduction and pyrite formation are complex (e.g., Berner, 1984, 1985), the relationship between concentrations of organic carbon and total reduced sulfur has been used to interpret paleoenvironments (e.g., Berner and Raiswell, 1983, 1984; Leventhal, 1983; Davison et al., 1985; Raiswell and Berner, 1985).

Three major types of environments may be discerned from the weight ratio of total organic carbon (TOC) to total reduced sulfur (TRS). Briefly, normal marine sediments have a ratio of about 2.8, while freshwater environments are expected to have higher ratios because of a lack of sulfate, and depressed C/S ratios are ascribed to anoxic environments, where sulfide is produced in the water column. However, a number of factors have emerged in some studies that complicate or invalidate the use of C/S ratios in paleoenvironmental reconstructions. These factors include (1) post-depositional mobility of reactive components (e.g., Berner, 1969; Morse et al., unpubl. data), (2) limitation of iron sulfide formation because of limitations in the available "reactive" iron (e.g., Canfield, 1988), (3) variations in the type of organic matter (e.g., Westrich and Berner, 1984), and (4) loss of organic matter during thermal maturation (Raiswell and Berner, 1987). In addition, this approach to environmental reconstruction seems questionable in sediments that are both low (<1 wt.% TOC; Raiswell and Berner, 1985) and high (>3 wt.% TOC; Morse et al., unpubl. data) in organic carbon.

The primary objective of this study is to determine the relationship of TOC to TRS in sediments from the Peru

upwelling area, as well as outline the factors that influence this ratio. The sediments of forearc basins on the shelf and slope are unusually rich in organic matter of marine origin (e.g., Powell et al., this volume), accumulate at high rates (in excess of 40 m/m.y.), and are thermally immature. Seifert et al. (this volume) found that carbon in amino compounds and carbohydrates—excellent substrates for bacterial metabolism—amount to a minimum of approximately 2% of TOC at depths below 20 meters below seafloor (mbsf), after decreasing rapidly from approximately 20% at the sediment/water interface. The experimental results of Parkes et al. (this volume) on microbial reduction of radio-labeled sulfate in samples from 90 mbsf further show that organic matter in the Quaternary diatomaceous muds and oozes from the shelf and upper slope is labile and contains abundant degradable substrate.

Added interest comes from the discovery of unusual subsurface hydrology in the study area (Kastner et al., this volume), which could pertain to the formation of reduced sulfur minerals. Our study complements earlier investigations of TRS in immature marine sediments from the Benguela upwelling system and the Tyrrhenian Sea (Morse et al., unpubl. data).

Geological and Depositional Settings of Sites 680 and 688

We chose to investigate Ocean Drilling Program (ODP) Sites 680 and 688, drilled during Leg 112, because the sediments recovered there conform to deposits of primary upwelling-related deposition on the shelf (Site 680) and to the secondary depositional center on the lower slope, where material that was resuspended on the shelf and upper slope has been redeposited (Site 688; Fig. 1). Organic-carbon-rich diatomaceous oozes and muds accumulated at both sites throughout the Pleistocene to Holocene, but differences in facies, in accumulation rates, and in the diagenetic boundary conditions of these coeval sediment sequences create differences in the paragenesis of diagenetic minerals and in the extent of organic-matter degradation by sulfate reduction. Older sediments (upper Miocene to Pleistocene at Site 680, Eocene to Pliocene at Site 688) are less organic-carbon-rich, contain more clastic components, and are coarser-grained at

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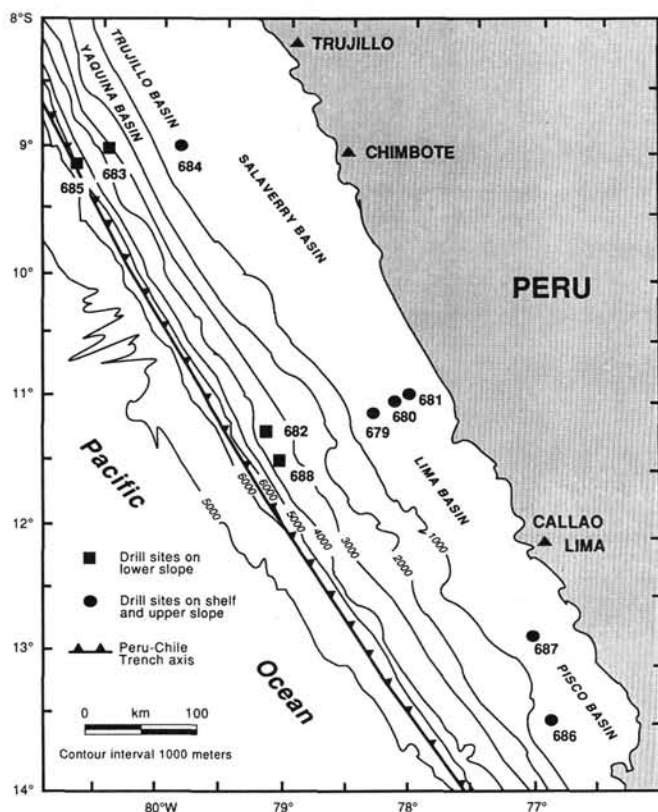


Figure 1. Location of Leg 112 drill sites offshore Peru with morphology and location of major forearc basins.

both sites; analysis of the carbon to sulfur relationship in the deeper parts of both sections might be suitable for evaluating the influences of physical properties and the peculiar hydrographic situation in the subsurface (see below) on diagenetic mineral formation. Because of problems with assessing C/S ratios in organic-lean sediments and because of different ages for the clastic intervals at both sites, we decided to concentrate this investigation on the Quaternary sections of lithologic Units I at Sites 680 and 688. We would like to point out, however, that TRS concentrations appeared inordinately high in the organic-lean sands and muds of both sites, and resulted in C/S ratios that were frequently below unity. This may indicate that increased permeability creates favorable conditions for pyrite precipitation at sites of enhanced lateral fluid migration.

Site 680 (Figs. 1 and 2) is located in a water depth of 250 m in the center of a lens-shaped accumulation of organic-carbon-rich upwelling sediments. Lithologic Units I and II (0.0 to 56.5 mbsf) are composed of foraminifer-bearing diatomaceous mud and ooze having alternating laminated and massive intervals; the sedimentation rate of Units I and II is approximately 55 m/m.y. Unit III (56.5 to 195.5 mbsf) is composed of sand, phosphatic sand, and mud. Laminated and diatomaceous intervals occur as intercalations of several meters thickness. Sedimentation rates in Unit II were about 30 m/m.y. and exceeded 100 m/m.y. in the lower Unit III (Suess, von Huene, et al., 1988).

A striking observation at Site 680, which was similarly encountered at all other sites on the shelf offshore Peru, was the discovery of a hypersaline subsurface brine that pro-

vided dissolved ions (all major ions except alkalinity increase downhole; Kastner et al., this volume) to fuel continued, extreme diagenesis in the organic-carbon-rich sediments. After depletion of interstitial sulfate at approximately 50 mbsf, sulfate concentrations increased to values of 37.9 mM/dm³ at 195.5 mbsf, thus driving bacterial sulfate reduction beyond its normal extent and creating unique diagenetic environments.

Site 688 (Figs. 1 and 3) is located on the lower slope seaward of Site 680 in a water depth of 3820 m. The lithologic units recognized here record progressive subsidence of Site 688 since the Eocene. Lithologic Unit I (0.0–338.5 mbsf) is of Pleistocene age and is composed of bioturbated diatomaceous mud. Sediments between 82.2 and 570 mbsf were black, but changed color to olive-gray after a few minutes of exposure to air. This phenomenon was interpreted as indicating the presence of metastable iron monosulfide, an observation that agrees with the extremely high sedimentation rates of 100 to 350 m/m.y. and the concomitant early depletion of sulfate in sediments having high iron contents (Bernier, 1974). Upwelling-related sedimentation of diatomaceous ooze and mud is recorded since the early Miocene in lithologic Unit II (338.5 – 593.0 mbsf), which was deposited at rates of 10 to 50 m/m.y. Lower to middle Eocene opal-free calcareous and clastic rocks of Unit III make up the remainder of the recovered section below a pronounced unconformity at the base of Unit II. Details on the chemical composition and origin of the unusual interstitial waters at Site 688 are presented by Kastner et al. (this volume).

MATERIALS AND METHODS

Samples (10 cm³) were taken from split cores on board the *JOIDES Resolution* based on a routine sample spacing of usually less than 3 m in the case of Hole 680A, 10 m in the case of Hole 688A, and much farther spaced in the clastic sediments low in organic carbon of Hole 688E (Tables 1 and 2). The samples were dried immediately in a freeze dryer, and then ground in an agate mortar. Calcium carbonate (CaCO₃) was determined using a Coulometrics CaCO₃ analyzer after acid treatment with 2N HCl. Organic carbon was determined with the TOC module of two different Rock-Eval pyrolysis instruments (Delsi Nermag): samples from Hole 680 were run on the shipboard instrument, and samples from Site 688 in a shore-based laboratory (Texaco, Houston). Both instruments were standardized using the standard material provided by Delsi. This procedure allowed us to establish the thermal maturity and state of preservation of the organic material in the samples by interpreting the hydrocarbon and carbon dioxide yields during pyrolysis, and by measuring the temperature of maximum hydrocarbon release during cracking of kerogen (or kerogen precursors). For the Rock-Eval technique, the reader should refer to Espitalié et al. (1985), Katz (1983), and Peters (1986), who also outline some pitfalls and precautions necessary when interpreting pyrolysis data from immature sediments. We found the method satisfactory for preliminary classification and evaluation of the state of degradation of organic matter in organic-rich (>2 wt.% TOC) immature sediments (Morse et al., unpublished data; Pratt et al., 1986).

The method for determining abundances of inorganic TRS is after Zhabina and Volkov (1978), as modified by Canfield et al. (1986). In brief, H₂S from reductive decomposition of sulfide by a Cr(II) solution in concentrated HCl is titrated with PbClO₄⁻, and the end point determined with a silver sulfide

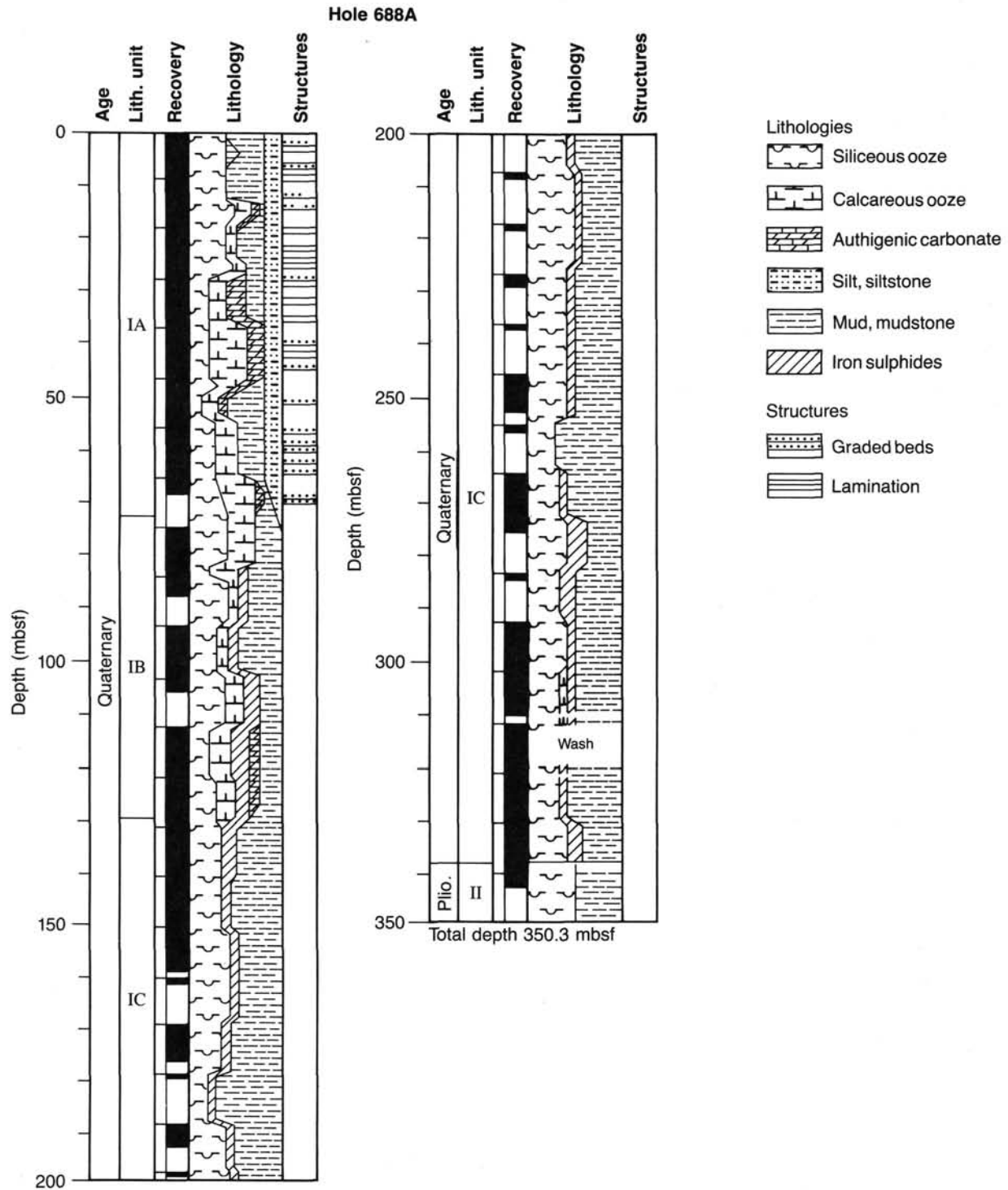


Figure 2. Lithologic summary of section recovered at Site 680.

reference electrode. Attempts to measure iron monosulfide (acid volatile sulfur, AVS) after digestion in cold 6N HCl (Westrich, 1983) failed, because AVS was not present above the detection limit of the method ($4 \mu\text{M/g}$), even though we strongly suspect that it was present in some of the fresh samples. Consequently, we interpret TRS and pyrite-S as being equivalent. The "reactive" iron fraction is a widely used and often loosely defined term that describes the fraction of total iron that probably is available for participation in

chemical reactions under early diagenetic conditions. Leaching procedures using citrate, dithionite, and HCl solutions of different strengths have been the most widely used to determine this fraction, but many other methods are also being used. Canfield (1988) conducted a careful study of the behavior of different iron phases and his results indicate that the citrate/dithionite method extracts all the major iron oxide phases, while it removes only minor lattice-bound iron from iron silicate minerals. One exception is the clay mineral

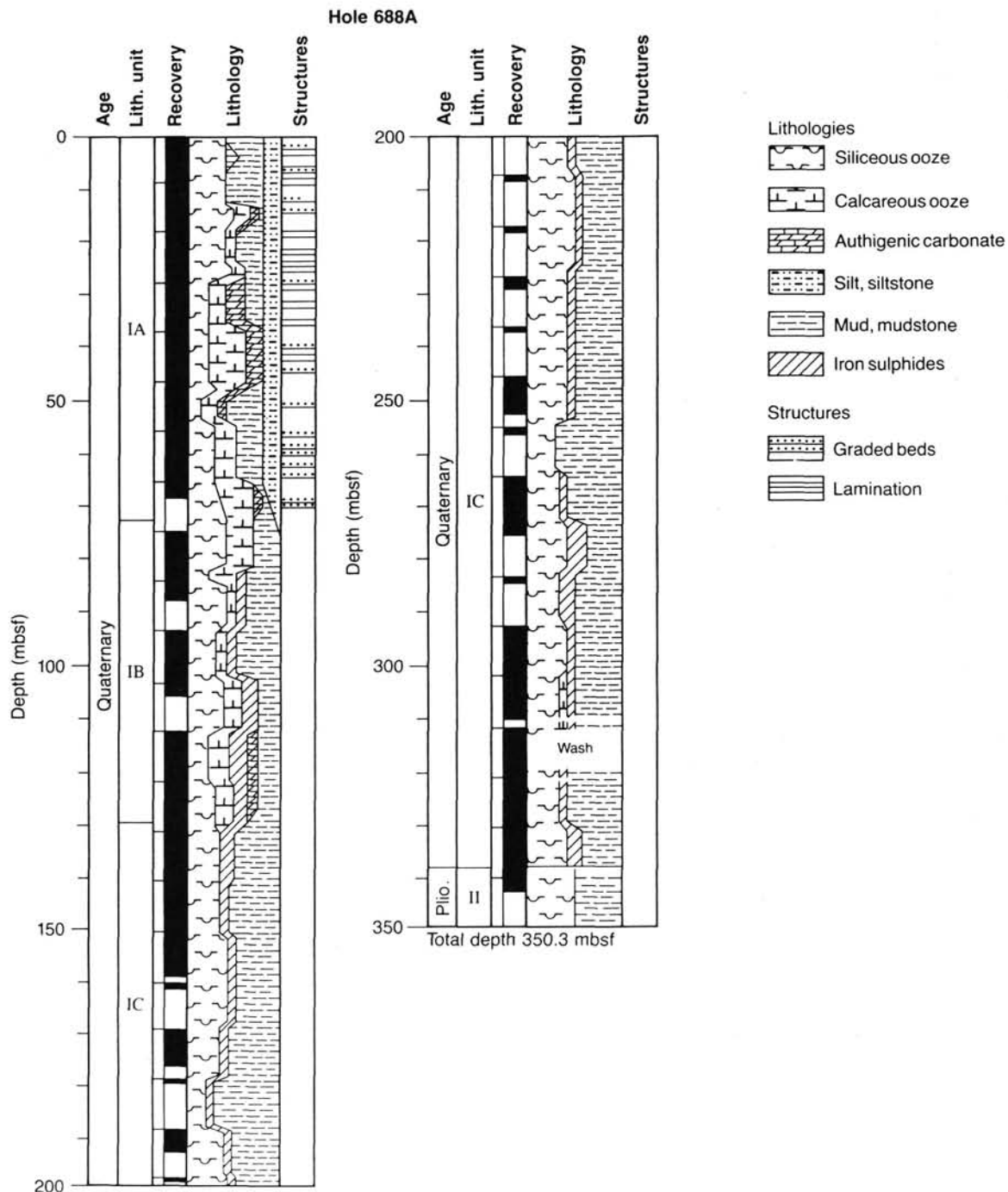


Figure 3. Lithologic summary of section recovered in Hole 688A.

nontronite. Huerta-Diaz and Morse (in press) compared the results for iron concentrations measured by both the citrate/dithionite method and by leaching with 1N HCl in sediments having varying iron contents; they found remarkably good agreement between the two methods. Therefore, we have chosen the 1N HCl-leachable iron to represent a reasonable approximation of the "reactive" iron fraction. The degree of pyritization (DOP) is given as

$$\text{DOP (molar ratio)} = \frac{\text{Pyrite}_{\text{Fe}}}{(\text{Pyrite}_{\text{Fe}} + \text{Reactive}_{\text{Fe}})},$$

where $\text{Pyrite}_{\text{Fe}}$ is well approximated as 0.5 TRS, based on the molar ratio of iron and sulfur in pyrite.

RESULTS

Concentrations of CaCO_3 , TOC, TRS, "reactive" iron (sol. Fe), total iron (von Breyman et al., this volume), DOP, C/S weight ratios, and pyrolysis indexes are listed in Tables 1 and 2. In the pyrolysis section of these tablets, T_{max} denotes the temperature of maximum hydrocarbon release from cracking of kerogen (or kerogen precursors), while HI and OI are the amounts of hydrocarbon and CO_2 , respectively, released from and normalized to the TOC content of the sample. These indexes are widely used to characterize the origin of organic matter in thermally mature sediments (Espitalié et al., 1985)

Table 1. Results of chemical analyses of Site 680 sediments.

Core, section, interval (cm)	Depth (mbsf)	CaCO ₃ (wt. %)	TOC (wt. %)	T _{max} (°C)	S ₁ (mg/g sediment)	S ₂	S ₃	HI	OI	TRS (wt. %)	Sol. Fe (wt. %)	Total Fe (wt. %)	DOP	C/S (Ratio)
112-680A-1H-2, 25-26	1.75	n.d.	2.18	403	1.24	7.54	3.19	345	146	n.d.	n.d.	n.d.	n.d.	n.d.
1H-2, 89-90	2.40	0.75	12.42	399	25.25	92.17	34.12	742	274	0.77	0.12	1.93	0.85	16.1
1H-3, 25-26	3.25	5.58	5.20	393	4.19	21.94	4.99	421	95	n.d.	n.d.	n.d.	n.d.	n.d.
1H-4, 25-26	4.75	4.17	5.94	396	4.16	22.75	7.11	382	119	0.87	0.10	n.d.	0.88	6.8
1H-4, 77-80	5.27	0.50	6.89	394	6.09	25.61	6.07	371	88	0.63	0.13	2.17	0.81	10.9
1H-4, 88-90	5.38	6.16	5.62	397	4.82	24.57	5.94	437	105	0.74	n.d.	n.d.	n.d.	7.6
1H-5, 25-26	6.25	14.49	9.75	392	7.86	40.32	9.83	413	100	0.61	0.12	n.d.	0.81	16.0
1H-5, 81-83	6.81	9.50	5.82	403	4.57	25.45	5.59	437	96	0.65	n.d.	n.d.	n.d.	9.0
1H-6, 25-26	7.75	4.66	6.16	400	5.01	27.63	8.06	448	130	0.78	0.10	n.d.	0.87	7.9
1H-6, 37-39	7.90	1.83	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.78	n.d.	1.59	n.d.	n.d.
2H-1, 25-26	8.55	13.08	4.64	394	2.99	18.89	4.12	407	88	0.67	0.08	n.d.	0.88	6.9
2H-1, 86-88	9.16	12.00	5.01	406	4.79	26.39	6.42	526	128	0.84	n.d.	1.89	n.d.	6.0
2H-2, 25-26	10.05	1.67	5.08	394	3.26	21.27	4.56	418	89	1.09	n.d.	n.d.	n.d.	4.7
2H-2, 96-98	10.76	31.99	3.38	401	1.94	12.35	3.04	365	89	1.14	0.13	3.96	0.87	3.0
2H-3, 25-26	11.55	2.42	8.83	392	6.55	37.05	7.55	419	85	0.84	0.10	n.d.	0.89	10.5
2H-3, 51-53	11.81	0.58	6.86	390	6.59	34.51	5.97	503	87	0.94	n.d.	2.30	n.d.	7.3
2H-4, 25-26	13.05	0.00	7.12	385	4.67	30.35	5.13	426	72	1.07	0.14	n.d.	0.87	6.7
2H-4, 56-58	13.36	0.42	3.65	397	3.07	23.03	4.63	630	126	0.79	n.d.	2.52	n.d.	4.6
2H-5, 25-26	14.55	11.83	2.94	414	1.88	11.79	2.88	401	97	0.92	0.10	2.50	0.89	3.2
2H-6, 25-26	16.05	0.08	3.47	402	3.46	24.71	3.75	712	108	0.96	0.11	2.07	0.89	3.6
2H-6, 68-70	16.38	0.33	3.16	406	2.63	23.89	3.52	756	111	1.21	n.d.	2.41	n.d.	2.6
2H-6, 77-80	16.48	0.48	1.04	404	0.87	8.09	2.53	777	243	0.71	0.12	n.d.	0.84	1.5
2H-7, 25-26	17.55	9.16	9.09	403	9.97	57.32	8.70	630	95	0.92	n.d.	n.d.	n.d.	9.9
2H-7, 44-46	17.74	15.25	4.54	390	8.45	42.63	6.99	939	153	1.00	0.11	2.35	0.89	4.5
3H-1, 26-27	18.05	9.00	2.95	412	1.31	8.37	2.44	285	83	0.91	n.d.	n.d.	n.d.	3.2
3H-1, 93-95	18.80	14.74	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.94	0.10	2.29	0.89	n.d.
3H-2, 26-27	19.55	3.76	3.77	412	4.3	28.57	5.61	757	148	0.75	n.d.	1.42	n.d.	5.0
3H-2, 121-123	20.46	0.25	3.96	402	5.83	35.02	6.50	884	164	0.74	0.10	n.d.	0.86	5.4
3H-3, 26-27	21.05	6.33	1.28	428	0.28	3.79	1.53	296	119	0.36	n.d.	n.d.	n.d.	3.6
3H-3, 116-118	21.96	10.75	7.26	400	8.45	42.10	8.69	585	120	0.96	0.10	2.06	0.89	7.6
3H-4, 26-27	22.55	1.00	5.80	413	5.36	40.40	7.36	696	126	0.84	n.d.	1.36	n.d.	6.9
3H-4, 119-121	23.49	0.67	8.42	386	6.62	26.58	5.18	315	11	1.20	0.12	n.d.	0.90	7.0
3H-5, 26-27	24.05	0.00	2.81	406	2.49	17.03	2.56	606	91	1.21	n.d.	n.d.	n.d.	2.3
3H-5, 32-34	24.12	3.17	4.07	404	1.17	8.79	2.84	215	69	1.01	0.13	2.57	0.87	4.0
3H-6, 26-27	25.55	26.49	2.00	425	0.19	2.34	1.29	117	64	0.18	n.d.	1.82	n.d.	11.1
3H-6, 81-83	26.11	0.17	7.37	412	4.46	48.58	7.26	659	98	0.73	0.09	n.d.	0.88	10.1
3H-7, 26-27	27.05	18.16	4.17	403	4.15	28.51	6.36	683	152	0.77	n.d.	1.93	n.d.	5.4
4H-1, 25-26	27.55	29.82	3.89	411	2.04	15.56	4.12	400	105	0.41	0.05	1.91	0.87	9.5
4H-2, 25-26	29.05	27.66	5.70	407	5.04	42.34	4.49	742	78	0.63	n.d.	1.71	n.d.	9.0
4H-3, 25-26	30.55	0.17	10.09	401	5.99	43.12	4.45	427	44	1.07	0.14	2.56	0.87	9.4
4H-4, 25-26	32.05	0.67	7.35	399	5.45	35.59	4.75	484	64	0.92	n.d.	1.93	n.d.	8.0
4H-5, 25-26	33.55	7.25	2.24	421	0.59	7.54	2.23	336	99	0.41	0.08	1.27	0.81	5.5
4H-6, 25-26	35.05	20.66	2.88	413	1.79	15.38	3.33	534	115	0.62	0.11	1.84	0.84	4.6
4H-7, 25-26	36.55	0.00	3.71	405	2.41	21.36	2.86	575	77	0.94	n.d.	2.33	n.d.	3.9
5H-1, 18-19	36.98	4.83	4.72	398	3.1	22.71	3.07	481	65	0.91	0.12	2.10	0.87	5.2
5H-2, 18-19	38.48	2.50	8.23	387	6.18	33.63	4.50	457	54	1.05	n.d.	2.10	n.d.	7.8
5H-3, 18-19	39.98	0.92	3.26	402	1.7	12.45	2.17	381	66	0.77	0.22	n.d.	0.75	4.2
5H-3, 57-59	40.40	7.33	10.16	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	1.29	n.d.	2.93	n.d.	7.9
5H-4, 18-19	41.47	0.17	6.24	388	4.65	27.35	4.32	438	69	0.99	0.13	1.85	0.87	6.3
5H-5, 18-19	42.96	2.17	5.44	396	2.98	26.40	4.37	485	80	0.98	n.d.	3.39	n.d.	5.6
6H-1, 18-19	46.38	3.84	4.40	385	3.83	20.10	2.60	456	59	1.23	0.11	2.50	0.90	3.6
7H-1, 35-36	56.15	0.42	3.68	387	3.32	16.65	2.36	452	64	0.73	n.d.	1.35	n.d.	5.0
7H-2, 35-36	57.63	1.67	0.37	357	0.02	0.07	0.83	18	224	1.50	n.d.	n.d.	n.d.	0.2
7H-2, 80-82	58.10	1.75	1.60	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	1.60	n.d.	3.81	n.d.	1.0
7H-3, 35-36	59.14	6.75	2.09	329	0.02	0.10	0.70	55	388	1.81	n.d.	4.11	n.d.	1.2
7H-4, 35-36	60.64	4.42	2.17	385	0.08	0.33	0.95	n.d.	n.d.	1.89	0.16	3.86	0.91	1.1
7H-5, 35-36	62.13	3.67	2.74	335	0.11	0.41	0.88	141	303	1.94	n.d.	4.17	n.d.	1.4
7H-6, 35-36	63.63	n.d.	2.16	384	0.13	0.69	0.61	222	196	1.86	0.16	n.d.	0.91	1.2
8H-1, 34-36	65.65	2.45	2.71	389	0.23	1.10	1.25	169	192	1.80	n.d.	3.59	n.d.	1.5
8H-2, 34-36	67.15	4.83	4.20	377	0.59	1.92	0.85	252	111	1.56	n.d.	2.87	n.d.	2.7
8H-3, 34-36	68.65	1.36	5.02	387	1.17	4.77	1.30	309	84	1.81	0.17	3.40	0.90	2.8
8H-4, 34-36	70.13	1.25	5.04	381	1.33	5.02	1.40	274	76	1.66	n.d.	3.16	n.d.	3.0
8H-5, 34-36	71.66	0.42	6.13	383	1.8	6.37	1.44	326	73	n.d.	0.17	2.63	n.d.	n.d.
8H-6, 34-36	73.16	5.50	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	2.68	n.d.	n.d.
8H-7, 34-36	74.66	1.07	6.01	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.16	3.46	n.d.	n.d.
9H-1, 34-36	75.14	1.33	3.13	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	4.38	n.d.	n.d.
9H-2, 34-36	76.64	0.25	3.65	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.19	3.86	n.d.	n.d.
9H-3, 34-36	78.14	0.83	6.97	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	3.73	n.d.	n.d.

Table 2. Results of chemical analyses of sediments at Site 688.

Core, section, interval (cm)	Depth (mbsf)	CaCO ₃ (wt. %)	TOC (wt. %)	T _{max} (°C)	S ₁ (mg/g sediment)	S ₂	S ₃	HI	OI	TRS (wt. %)	Sol. Fe (wt. %)	Total Fe (wt. %)	DOP	C/S (Ratio)
12-688A-1H-5, 82-83	6.8	1.33	3.02	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.66	n.d.	3.58	n.d.	4.6
2H-1, 44-45	8.7	1.00	2.77	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	1.00	n.d.	4.03	n.d.	2.8
2H-3, 44-45	11.7	1.33	1.85	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.39	n.d.	2.96	n.d.	4.8
2H-5, 44-45	14.7	1.75	1.56	423	1.15	4.48	1.97	286	126	0.56	n.d.	3.22	n.d.	2.8
2H-7, 44-45	17.7	10.34	3.73	418	2.59	13.58	5.32	364	143	0.87	0.69	3.69	0.52	4.3
3H-2, 42-43	19.7	10.68	3.28	406	3.24	10.77	4.59	329	140	1.16	n.d.	3.36	n.d.	2.8
3H-4, 42-43	22.7	10.89	2.72	422	1.79	9.10	4.51	334	166	1.18	0.68	3.27	0.60	2.3
3H-4, 140-150	23.7	n.d.	1.99	424	0.68	5.07	2.58	254	129	1.14	0.64	n.d.	0.61	1.8
4H-3, 44-45	30.7	6.51	2.70	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.88	n.d.	3.49	n.d.	3.1
5H-3, 64-65	40.4	49.87	1.55	423	0.90	5.17	2.49	334	161	0.84	n.d.	4.19	n.d.	1.9
6H-2, 63-64	48.5	13.76	1.91	422	1.20	5.87	3.13	307	164	0.93	0.59	3.41	0.58	2.0
6H-3, 145-150	50.8	8.48	2.14	424	0.68	5.07	2.58	254	129	0.81	n.d.	3.19	n.d.	2.6
8X-1, 57-58	65.9	21.35	3.67	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	1.08	n.d.	3.19	n.d.	3.4
9X-5, 100-111	81.9	9.17	3.87	413	3.50	16.41	5.12	424	132	1.06	n.d.	3.08	n.d.	3.7
9X-5, 140-150	82.2	n.d.	4.73	418	2.16	16.37	3.94	346	83	1.34	0.80	n.d.	0.54	3.5
9X-6, 110-111	83.4	1.50	3.32	405	2.98	12.39	5.20	374	157	0.80	n.d.	2.70	n.d.	4.2
10X-2, 32-33	86.1	8.76	3.55	404	2.28	8.73	6.14	246	173	1.32	1.77	3.66	0.39	2.7
11X-2, 28-29	95.6	8.09	3.76	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.86	n.d.	3.23	n.d.	4.4
12X-1, 55-56	103.9	8.59	4.24	414	3.50	17.37	6.04	410	143	0.68	1.06	2.95	0.36	6.2
13X-2, 66-67	115.0	5.34	3.67	420	2.28	13.60	4.77	370	130	0.55	1.34	3.58	0.26	6.7
13X-6, 66-67	121.0	11.84	3.56	419	2.29	12.94	5.41	364	152	0.73	n.d.	3.54	n.d.	4.9
14X-2, 85-86	124.7	8.84	3.76	414	2.46	12.79	7.37	340	196	0.73	1.94	4.17	0.25	5.2
14X-6, 85-86	130.7	4.34	4.08	417	2.82	15.56	6.24	381	153	0.32	n.d.	3.35	n.d.	12.6
16X-2, 11-12	142.9	0.32	4.40	413	3.18	15.23	5.83	346	132	0.68	1.29	3.12	0.32	6.4
16X-6, 12-13	148.9	2.50	4.87	419	3.48	19.87	5.94	408	122	0.52	1.30	3.30	0.26	9.3
17X-1, 58-59	151.4	3.50	3.36	416	2.50	13.38	5.95	398	177	0.79	n.d.	3.79	n.d.	4.3
17X-6, 58-59	158.9	2.75	3.53	421	2.24	13.88	4.79	393	136	0.52	1.45	3.48	0.24	6.8
18X-1, 133-135	161.6	4.17	4.78	413	3.88	18.65	6.30	390	132	0.67	n.d.	3.10	n.d.	7.2
19X-1, 58-59	170.4	8.59	3.71	419	2.27	14.67	5.71	395	154	n.d.	1.56	3.88	0.28	n.d.
19X-3, 140-150	174.2	n.d.	3.24	424	0.88	10.35	3.51	319	108	0.48	1.83	n.d.	0.19	6.7
19X-5, 58-59	176.4	7.26	2.80	416	1.49	9.91	4.65	354	166	0.90	n.d.	4.12	n.d.	3.1
21X-1, 63-64	189.4	14.68	3.53	409	2.47	12.21	6.86	346	195	0.68	1.63	3.35	0.27	5.2
21X-3, 63-64	192.4	8.17	3.09	410	1.90	9.86	5.27	319	170	1.00	n.d.	3.63	n.d.	3.1
21X-3, 108-118	192.9	n.d.	3.41	417	1.05	9.86	3.33	289	97	1.01	n.d.	n.d.	n.d.	3.4
22X-1, 20-21	198.5	9.67	5.75	415	4.43	24.28	7.19	422	125	0.89	n.d.	3.16	n.d.	6.4
23X-1, 69-70	208.5	2.92	3.38	418	2.36	14.34	4.72	424	140	0.69	1.15	3.05	0.34	4.9
24X-1, 50-51	217.8	2.00	4.79	416	3.45	19.57	4.99	409	104	1.06	n.d.	3.33	n.d.	4.5
25X-1, 62-63	227.4	1.83	8.00	408	7.74	35.38	7.38	442	92	0.95	0.90	2.56	0.48	8.4
26X-1, 33-34	236.6	1.42	5.17	409	4.20	21.03	5.21	407	101	0.85	0.27	2.91	0.73	6.1
27X-1, 25-26	246.1	1.08	3.24	414	2.57	12.73	3.71	393	115	1.04	n.d.	3.55	n.d.	3.1
27X-4, 140-150	251.7	n.d.	2.71	413	1.36	16.66	3.27	614	120	1.60	0.71	n.d.	0.66	1.7
28X-1, 55-56	255.9	1.92	4.99	423	2.36	17.36	7.00	348	140	1.26	n.d.	3.12	n.d.	4.0
29X-2, 38-39	269.7	1.10	5.44	410	4.15	23.64	4.91	435	90	1.00	n.d.	3.02	n.d.	5.5
30X-1, 39-40	277.8	1.85	4.78	410	3.61	18.68	5.01	391	105	1.14	1.46	3.45	0.40	4.2
31X-1, 39-40	287.4	n.d.	4.49	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	0.75	n.d.	3.03	n.d.	6.0
32X-1, 37-38	297.0	3.76	3.38	417	2.10	13.20	4.90	390	145	0.95	1.68	4.13	0.33	3.6
33X-1, 86-87	303.7	3.43	4.64	415	2.91	18.68	5.58	402	120	0.71	n.d.	2.74	n.d.	6.6
34X-1, 68-69	313.0	1.75	4.51	407	4.17	20.46	4.25	454	94	0.27	n.d.	3.51	n.d.	16.8
36X-1, 85-86	332.2	1.75	3.75	416	2.69	15.85	3.50	422	93	1.12	1.02	3.73	n.d.	3.4
36X-6, 140-150	339.9	n.d.	3.72	427	1.15	15.81	2.78	425	74	1.04	n.d.	n.d.	n.d.	3.6
37X-2, 59-61	342.9	1.00	6.93	402	7.07	31.54	5.93	456	86	0.11	0.71	2.75	0.11	65.4
12-688E-3R-3, 72-73	368.7	n.d.	4.02	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.	1.15	n.d.	n.d.	n.d.	3.5
3R-4, 140-150	370.9	1.25	4.19	391	2.42	18.88	3.21	451	77	0.23	0.20	n.d.	n.d.	18.2
6R-4, 140-150	399.4	2.67	2.20	397	0.96	9.07	1.90	412	86	1.00	0.22	n.d.	n.d.	2.2
9R-5, 140-150	429.4	1.67	2.35	400	1.18	9.12	1.65	388	70	0.97	n.d.	n.d.	n.d.	2.4
12R-1, 140-150	451.9	3.92	3.92	401	1.84	16.96	3.55	433	91	0.77	n.d.	n.d.	n.d.	5.1
19R-3, 140-150	521.2	4.75	1.88	417	0.36	6.90	1.37	367	73	0.57	0.18	n.d.	n.d.	3.3
23R-1, 140-150	556.4	18.58	0.86	413	0.21	2.11	1.69	245	197	0.51	0.84	n.d.	n.d.	1.7
27R-1, 140-150	594.4	1.75	0.39	412	0.05	0.48	0.53	123	136	0.99	0.53	n.d.	n.d.	0.4
30R-1, 140-150	622.9	3.17	0.25	409	0.05	0.23	0.66	92	264	0.49	n.d.	n.d.	n.d.	0.5
33R-1, 140-150	651.4	10.25	0.00	n.d.	0.02	0.00	0.18	n.d.	n.d.	0.12	2.28	n.d.	n.d.	0.0
35R-1, 140-150	670.4	3.75	0.65	417	0.08	0.75	0.43	115	66	0.89	n.d.	n.d.	n.d.	0.7
37R-1, 140-150	689.4	4.66	0.83	423	0.04	1.49	0.73	180	88	0.62	1.97	n.d.	n.d.	1.3
43R-4, 87-97	750.4	4.41	1.35	418	0.12	3.87	0.87	287	64	0.92	n.d.	n.d.	n.d.	1.5

and are applicable to immature (T_{max} below 425°C) marine sediments with organic-carbon values above 2 wt.% as an indicator of provenance and state of degradation (e.g., Pratt et al., 1986).

The T_{max} values of pyrolytic hydrocarbon yield are below the lower threshold of the "oil window" (425°C) and reflect thermal immaturity of the organic matter in both holes. TOC averages 5.2 wt.% in Hole 680A. Values of HI in samples of Unit I of Hole 680A (Fig. 4) are highly variable and reach up to 900 at low OI.

Such a high mean value of HI of 504, combined with a low average OI of 103 (Table 3) shows that the organic carbon deposited in Unit I at Site 680 is of marine origin (Espitalié et al., 1985) and contains abundant hydrocarbons and labile material. This observation is substantiated by analyses of labile particulate amino acids and sugars in comparable and coeval sediments of Site 681 (Seifert et al., this volume). Samples of Unit III have low hydrogen content and can be plotted in the area of terrestrial organic matter.

Organic carbon in lithologic Unit I of Hole 688A (0–338.5 mbsf) was deposited during the Quaternary, seaward of Site 680, and contains redeposited material from the shelf and upper slope. Both inorganic and organic geochemical characteristics of the sediments are different in lithologic Units I of the two sites. The variability in HI and OI is much less obvious in Hole 688A, which is confined to a narrow area between evolution paths of Type II and Type III organic matter. Pratt et al. (1986) found that HI and OI values of laminated and bioturbated interlayers in marine sediments differ significantly, because hydrogen loss during oxidation of marine organic matter in bioturbated layers results in a shift to lower HI and higher OI. Such oxidized marine organic matter is intermediate between the evolution paths of marine and terrestrial organic matter in a plot of HI and OI, an effect that can be seen in samples of Hole 688A.

The elimination of substrate availability as a limiting factor for pyrite formation leaves sulfate and "reactive" iron limitations as possible reasons for the unexpected similarity in TRS concentrations in the sediments of the Peru margin. We plotted TOC, TRS, and the concentration of the "reactive" iron in Holes 680A, 688A, and 688E vs. depth in Figures 5 and 6. Average values of TOC and TRS are 5.23 wt.% and 0.85 wt.%, respectively, and the C/S ratio of these averages is 6.1. This is about twice the normal marine ratio of 2.8. Because Site 680 is located on the shelf and is supplied with sulfate-bearing hypersaline fluids in the subsurface, the deeper section exhibits interesting trends in C/S ratio, sulfate gradient, and degree of pyritization. The latter value is high throughout the upper section to 56 mbsf (average for lithologic Unit I = 0.86), and exhaustion of "reactive" iron is probably responsible for the high C/S ratios. Samples from lithologic Unit III, the sandy, clastic-dominated nearshore facies, have low TOC concentrations and the highest TRS content (average = 1.8 wt.%) of all samples studied (Fig. 5). In the three samples from this interval, the degree of pyritization is inordinately high (average = 0.91%) and points to severe depletion of "reactive" iron. From the data on sulfate concentrations in pore waters given in Kastner et al. (this volume), it is obvious that sulfate reduction and H₂S production persists throughout the lithologic column at Site 680. TRS concentrations in lithologic Unit III are higher than in the organic-rich mudstones above, even though organic carbon in the clastic sediments is low. Consequently, C/S ratios are considerably lower than either in "normal" marine sediments (Sweeney, 1972), or in any of the other samples studied from this site. We propose that diffusion of H₂S and the "leaching" of iron bound in minerals of the clastic sequence of lithologic Unit III at Site 680 results in such high TRS concentrations. According to Mossman et al.'s results (this volume), dissolved sulfide in pore waters of Site 680 reaches 4.5 mM at 47 mbsf in Unit I and declines to 0.1 mM/dm³ at 72 mbsf in Unit III. The concentration gradient implies downward diffusion of sulfide from the level of maximum concentration within the organic-carbon-rich upwelling deposits to the clastic sediments of Unit II. We propose that the clastic sequence, where iron concentrations are on average higher than in the biogenic sediments above, is the site of pyrite formation from migrated sulfide, in spite of exhaustion of the "reactive" iron measured during our leaching method. The source of iron in the clastic sequence is not identified, but possible sources are magnetic minerals, such as magnetite, that have not decomposed by our extraction procedure, or iron diffusing upward from deeper in the section.

In contrast to Hole 680A, the Quaternary sediments in Hole 688A have a significantly lower degree of pyritization (average = 0.4) and a ratio of average TOC to TRS of 4.3

(Table 3). Note that in this comparison the means of both TOC and the HI of samples from Units I of Holes 680A and 688A are significantly different (at a 95% confidence level in a Student t-test). TRS concentrations are not significantly different and average 0.86 wt.% and 0.85 wt.% in Hole 688A and in Hole 680A, respectively. In a plot of TOC vs. TRS for lithologic Units I in Holes 680A and 688A, samples with TOC < 3 wt.% follow the normal marine C/S ratio of about 2.8, while samples containing more than 3 wt.% TOC deviate systematically (Fig. 7). HIs of samples from lithologic Units I at both sites are not significantly correlated with TRS, and exhaustion of organic substrate cannot have been the limiting factor for pyrite formation at either of the two sites.

A plot of TRS vs. DOP demonstrates the limitation of pyrite formation by "reactive" iron in Hole 680A (Fig. 8), where no correlation is apparent between the two parameters. "Reactive" iron, even as measured by our rather gentle leaching method, may overestimate the availability of iron for pyrite formation by about 8%, because the DOP never exceeds 0.92 even in the presence of interstitial sulfide in pore-water samples from this site (Mossman et al., this volume). We conclude that "reactive" iron is limiting the formation of iron sulfide in sediments from the shelf site, where pyrite concentration averages 1.6 wt.% and ranges from 0.34 to 2.3 wt.%. Iron in pyrite averages 0.74 wt.% (range of 0.15 to 1.06 wt.%), which is, on average, 35% of total iron (Table 1).

DOP values correlate positively with TRS in the case of samples from Hole 688A (Fig. 8); one surprising observation is that an extrapolated DOP value of 0.9 resulted in TRS concentrations similar to those in the clastic Unit II of Hole 680A. Iron in pyrite (average 0.74 wt.%, range of 0.23 to 1.38 wt.%) averages only 22% of total iron in sediments of Hole 688A (Table 2). Pyrite contributes, on average, 1.6 wt.% to the sediment, similar to the value found in Hole 680A.

The preceding observations imply that, because abundant "reactive" iron and organic carbon are available for pyrite formation in samples from Hole 688A, a third factor limits the formation of pyrite here. This third factor may be limitation by sulfate. All three samples from the upper 40 mbsf of Hole 688A, where sulfate was found in interstitial waters, and all samples above 80 mbsf (outside the zone where iron monosulfide occurred) show DOP values above 0.5, with roughly normal marine C/S ratios. Even though traces of sulfate (tenths of millimoles) were reported at depths below 100 mbsf (Suess, von Huene, et al., 1988), these low sulfate values may be artifacts of sampling (M. Kastner, pers. comm., 1988).

CONCLUSIONS

Reduced-sulfur accumulation in organic-carbon-rich sediments from the continental slope and shelf offshore Peru is influenced by several factors, including iron limitation in the nearshore environment of Site 680 and exhaustion of sulfate in the rapidly accumulating continental slope sediments of Site 688. Concentration and quality of organic matter (frequently the dominant control for reduced sulfur accumulation) are high and do not limit bacterial sulfate reduction. C/S ratios are mainly influenced by an upper concentration limit of approximately 1 wt.% TRS, and the variability of organic matter concentrations. Above 3 wt.% TOC, the amount of TRS does not increase, and C/S ratios reach a maximum value of about 16 at both sites. Average TRS concentrations are the same in sediments of Pleistocene age at both sites, even though sedimentation rates are different by a factor of 2. At Site 680,

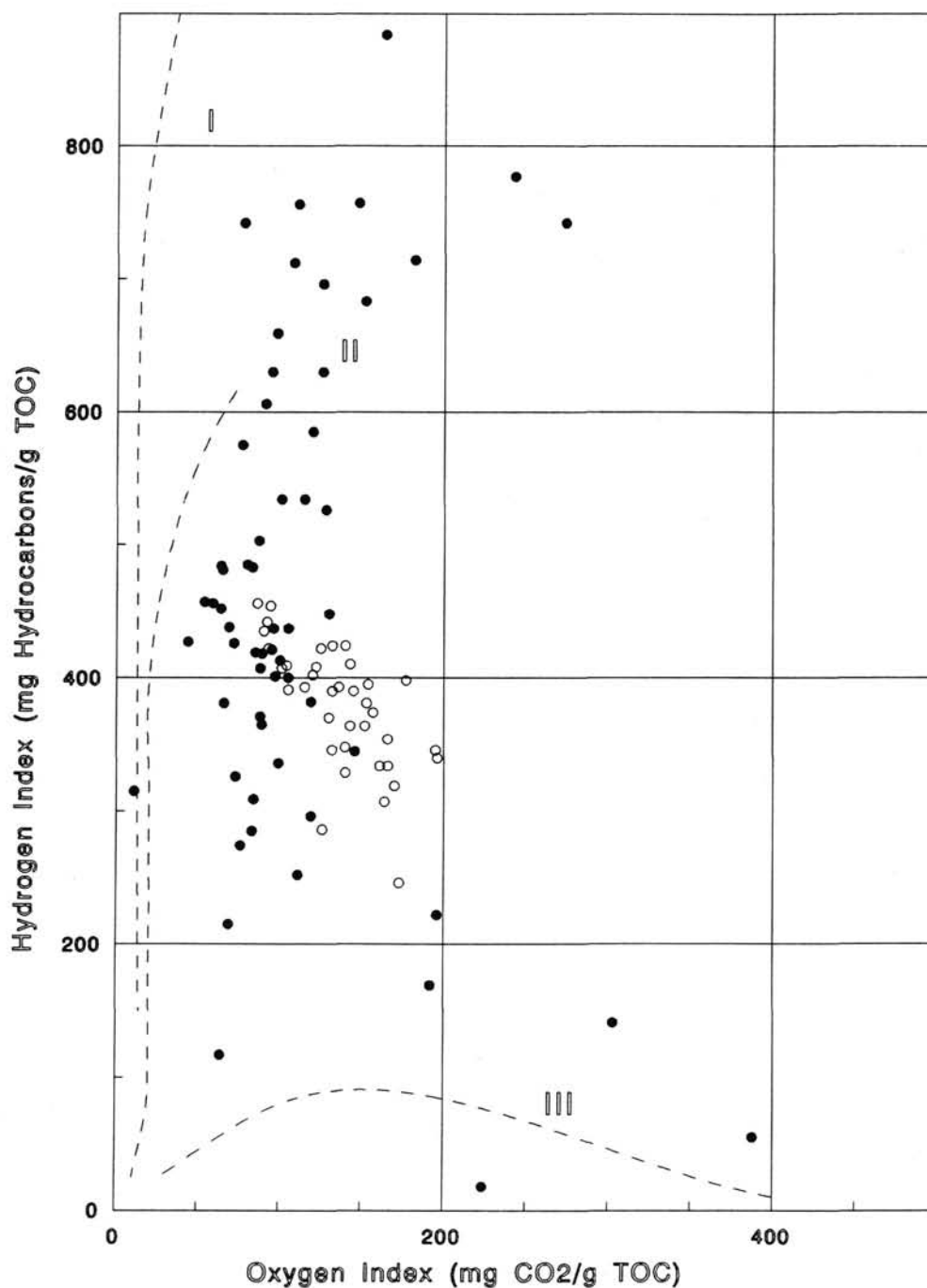


Figure 4. Van Krevelen-type diagram depicting the OI and HI of samples from Holes 680A (closed circles) and 688A (open circles). Evolution paths of kerogen Types I through III are denoted by dashed lines. Note the spread of HI for samples from Hole 680A, while samples from Hole 688 are well grouped and homogeneous.

the downward diffusion of sulfide, the subsurface supply of sulfate, and possibly the abundance of iron minerals that are not decomposed by our leaching technique lead to high TRS concentrations (up to 1.94 wt.%) in organic-matter-lean sediments of lithologic Unit III.

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Table 3. Statistical evaluation of results of chemical analyses for samples from lithologic Unit I at both Sites 680 and 688.

	N	Mean	Median	Std.dev.	SE	Min.	Max.
<i>Hole 680A:</i>							
CaCO ₃	50	6.99	3.80	8.48	1.20	0.00	31.99
TOC	48	5.23	4.86	2.45	0.35	1.00	12.42
HI	48	504	452	174	25.1	117	939
OI	47	103	95	45	6.6	11	274
TRS	49	0.85	0.87	0.23	0.03	0.18	1.29
DOP	26	0.86	0.87	0.04	0.007	0.75	0.90
<i>Hole 688A:</i>							
CaCO ₃	42	6.70	3.97	8.27	1.28	0.32	49.87
TOC	48	3.69	3.54	1.19	0.17	1.55	8.00
HI	41	371	374	65	10	246	614
OI	41	134	132	29	4	83	196
TRS	48	0.86	0.87	0.27	0.03	0.27	1.60
DOP	21	0.41	0.36	0.16	0.035	0.19	0.73

TOC = total organic carbon; TRS = total reduced sulfur; HI = hydrogen index; OI = oxygen index; DOP = degree of pyritization; Std. dev. = standard deviation; SE = standard error of the mean; Min. = minimum value; Max. = maximum value.

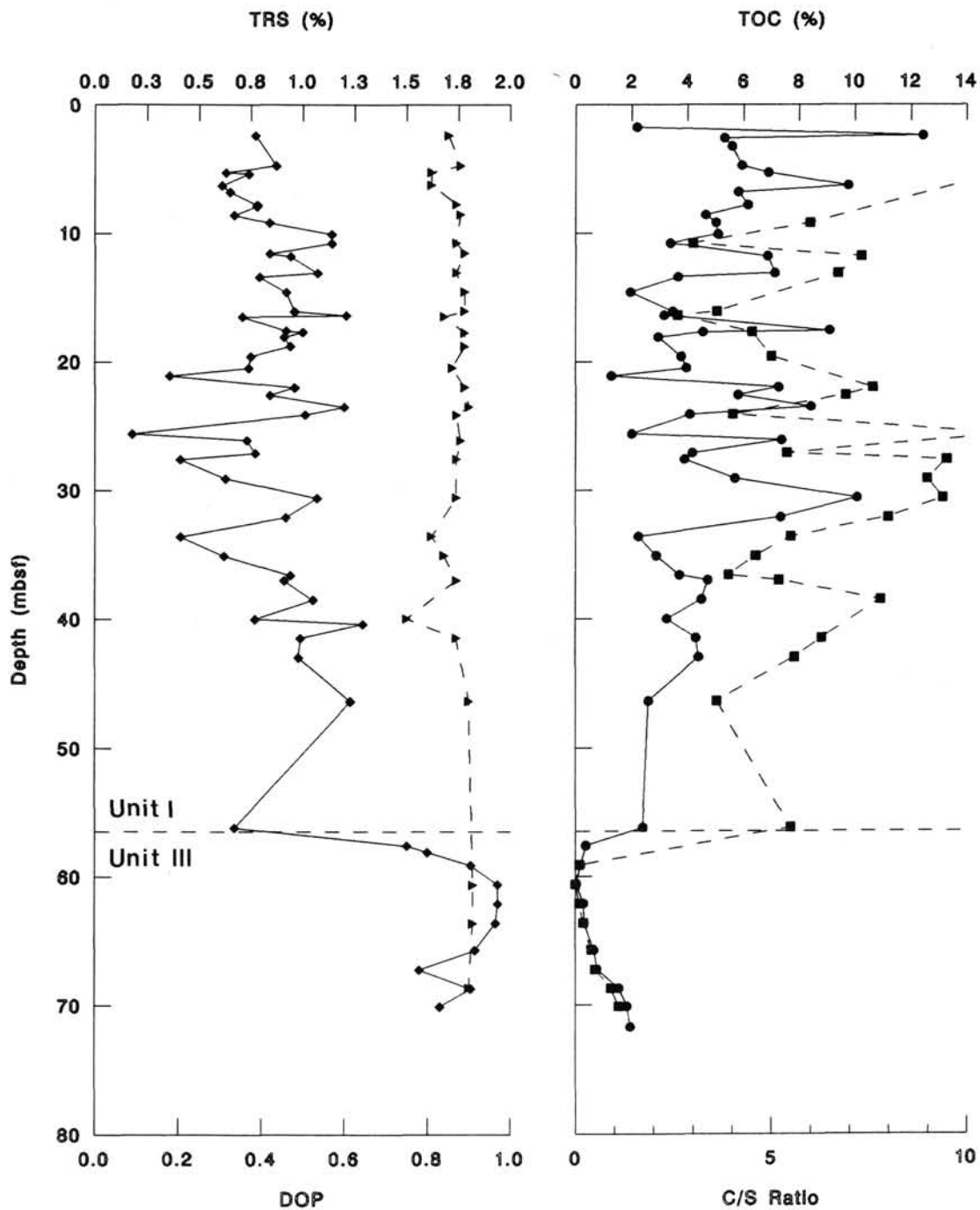


Figure 5. Downhole concentrations of TRS (solid line, diamonds), DOP (dashed line, triangles) TOC (solid line, closed circles), and C/S ratios (dashed line, squares) in Hole 680A.

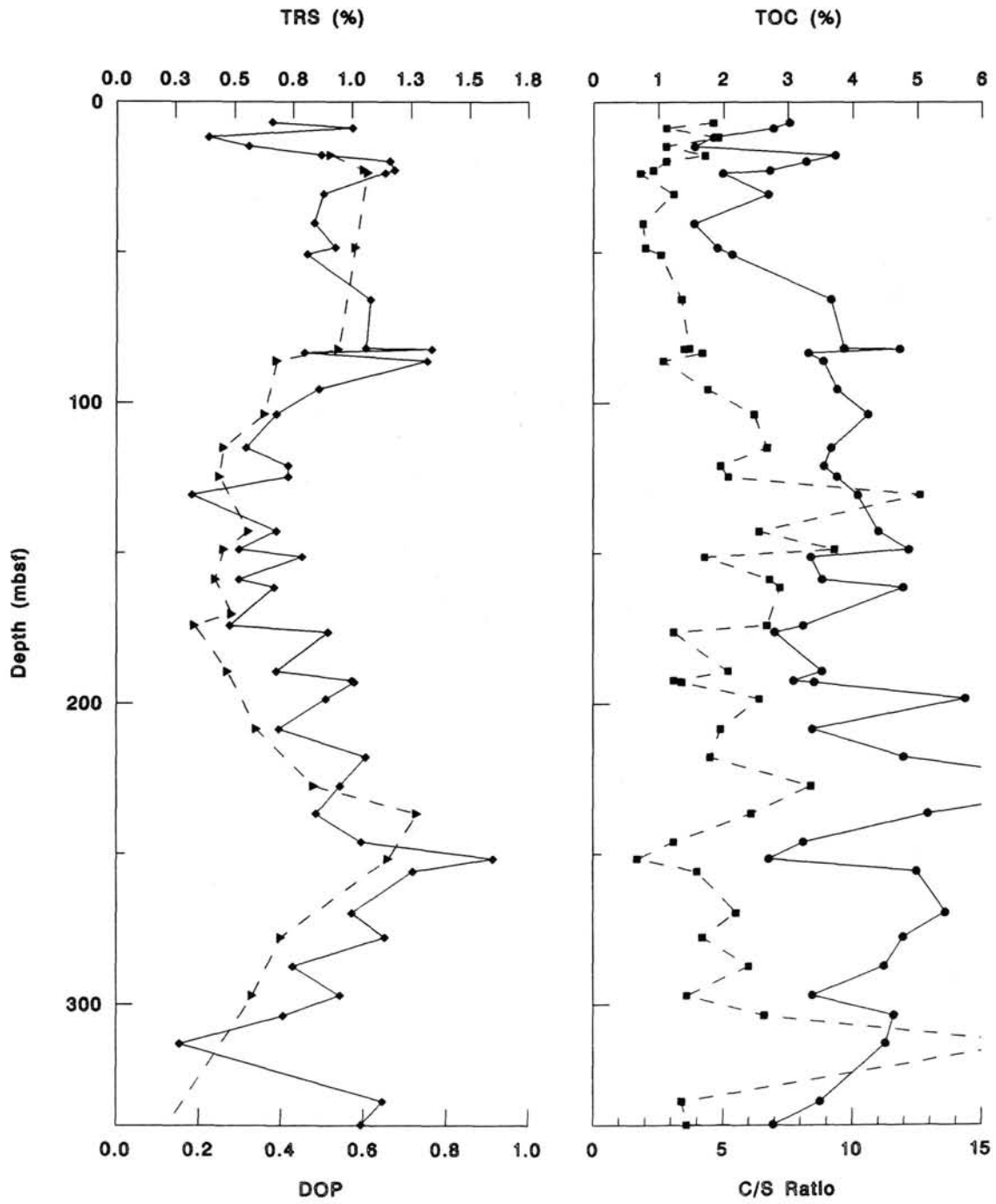


Figure 6. Downhole concentrations of TRS (solid line, diamonds), DOP (dashed line, triangles), TOC (solid line, filled circles), and C/S ratios (dashed line, squares) in Hole 688A, lithologic Unit I.

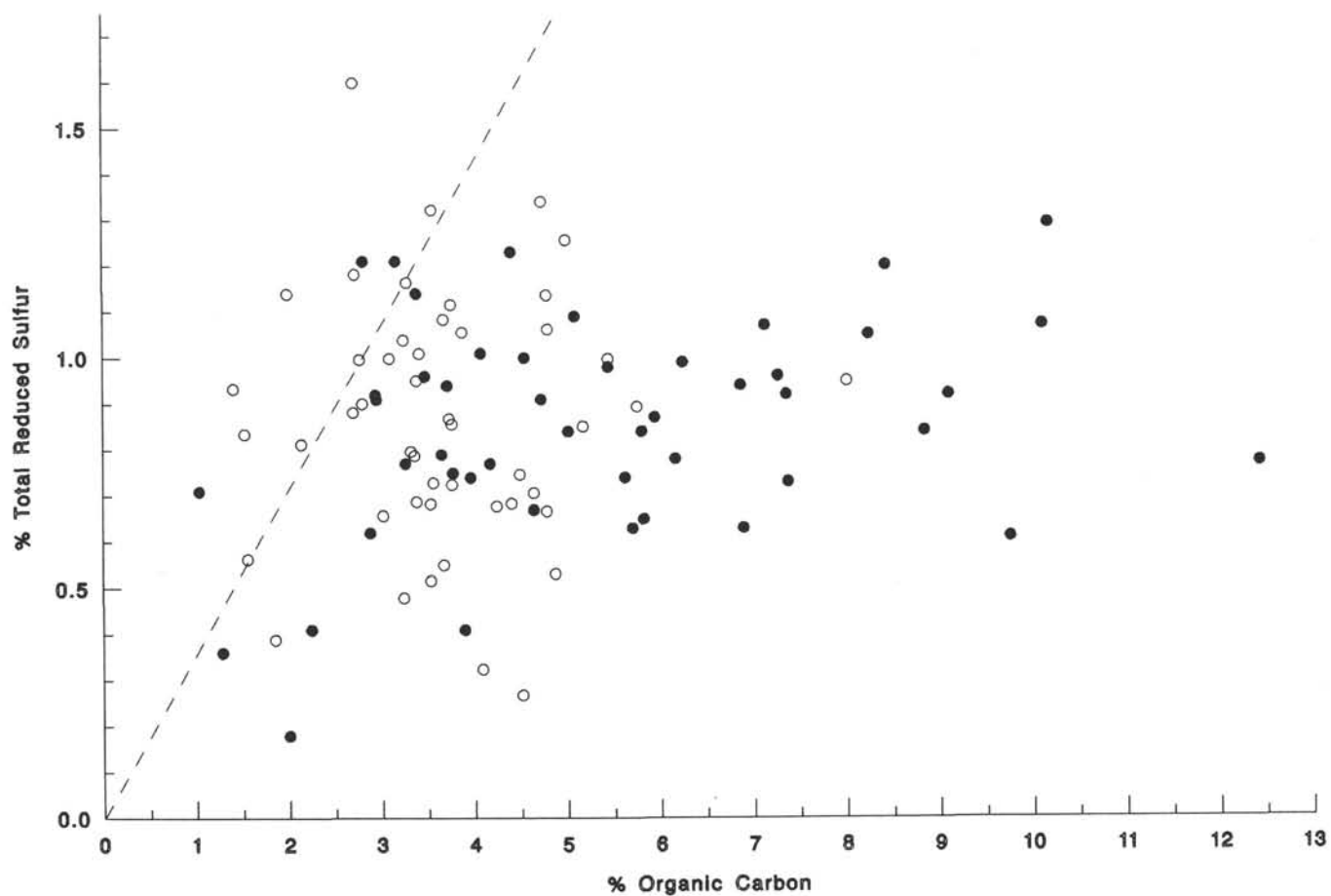


Figure 7. Plot of TOC vs. TRS for samples from Sites 680 (closed circles) and 688 (open circles) investigated here. The dashed line denotes a "normal" marine ratio of 2.8, as postulated by Sweeney (1972) and Berner (1984). Beyond 3 wt.% TOC, the ratio of C/S deviates systematically from the ratio because TRS concentrations do not increase at increasing TOC.

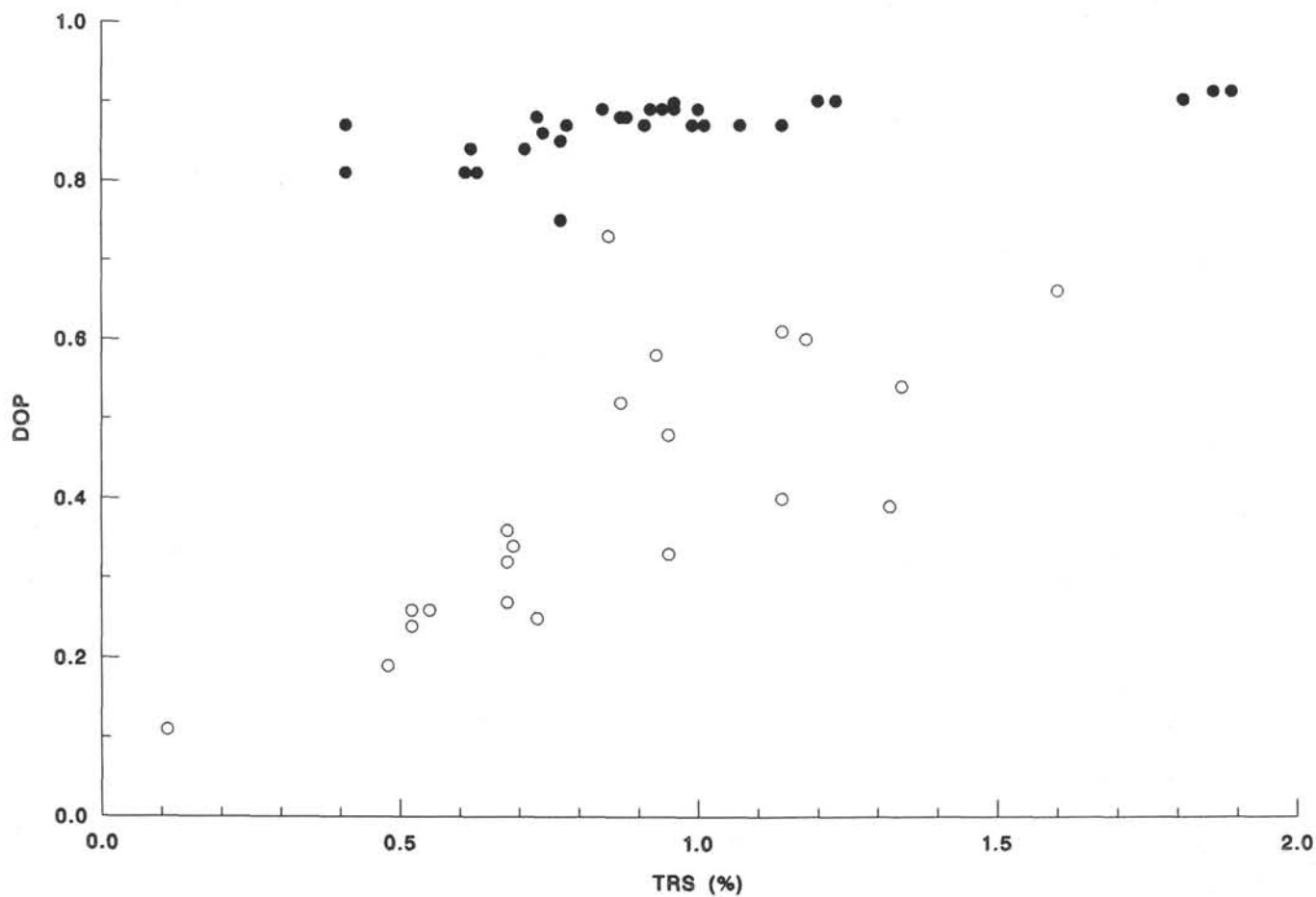


Figure 8. Plot of TRS vs. DOP for samples from Sites 680 (closed circles) and 688 (open circles). In Hole 680A, "reactive" iron is exhausted, and no correlation exists between TRS and DOP. Extrapolation of the relationship between TRS and DOP for samples from Hole 688A would result in TRS values of about 2 wt.% at DOP about 0.9, the same values as those encountered in samples of Unit II at Site 680. Note that DOP is high and C/S is low in samples from lithologic Unit IA of Hole 688A.